

H&H L6&7, MUST SKIM P124-165, but ASSIMILATE 134-138,156-162.

DO NOT DO 6-2, 6-3; 7-3b) & c), 7-4

... If extra time, go back & do any missed labs

## SHOW & TELL:

Heat sinks

Resistors: 1<sup>st</sup> 2-bands = std  $\pm 10\%$  values: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82

How FETs work

Please turn off everything upon leaving for the day (unlike AdLab, where stability critical).

Transistors: for low noise front ends, use Differential Amps vs. single-ended...

typical transistor current gain  $\beta \sim 100$

ac or dc

= an impedance multiplier/matcher:

emitter follower: impedance is  $\beta \times R_E$  emitter resistor

p96

$R_E$  provides negative feedback to stabilize gain; warm up xister w/two fingers.

common emitter input Z: =  $\beta \times R_C$  (collector resistor)

bias your xister “quiescently” to avoid saturation, clipping, distortion, etc.

input dynamic range, relative to  $0.6 V_{BE}$ , otherwise xister is not active

output voltage compliance

see p140, “Jargon”

= output voltage dynamic range of current source

...limited by the 2 rails, typically ground, and  $\pm 5$ ,  $\pm 6$ ,  $\pm 12$ ,  $\pm 24$ vdc (why $\pm$ ?)

$i_S$  saturation current,  $R_C$  limits output current

FET (Field Effect Transistor) “ $\beta$ ” > 1000...the front-end that’s hidden inside all op amp ICs.

Pretty simple: current amplifier:  $I_C = \beta \cdot I_B$

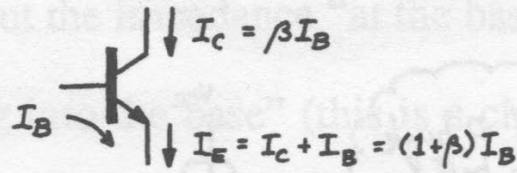


Figure N4.2: Transistor as *current-controlled valve or amplifier*

Very simple: say nothing of Beta (though assume it's at work)

- Call  $V_{BE}$  constant (at about 0.6 v);
- call  $I_C = I_E$ .

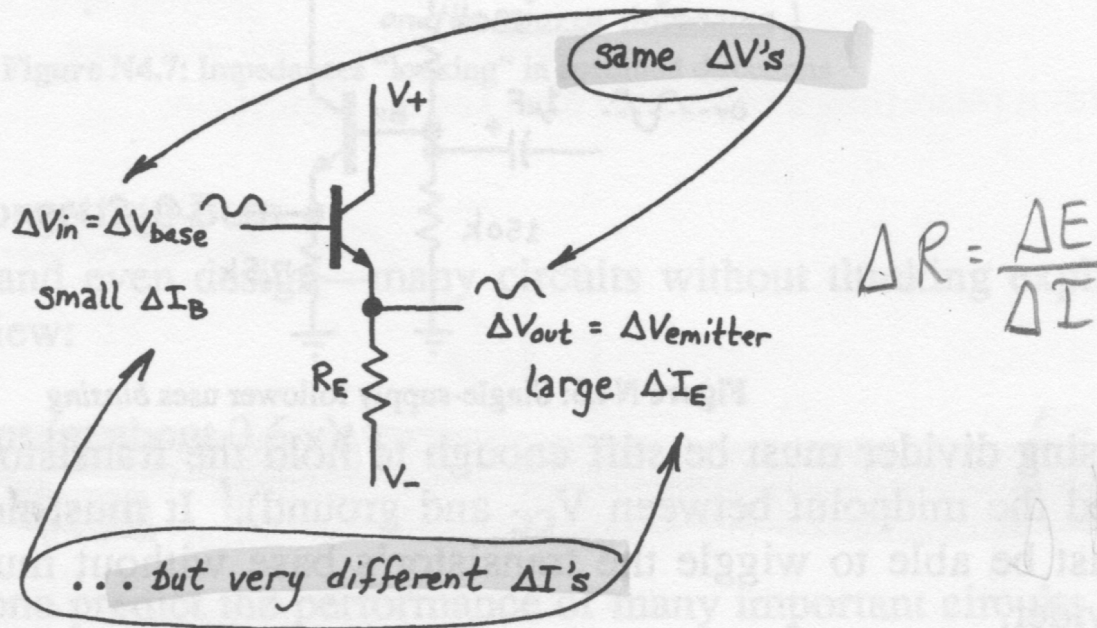


Figure N4.3: How a follower changes impedances

## RECIPE FOR COMMON-EMITTER PIE

What output current do you want to drive?

With quiescent  $V_{out} \sim 1v$ , need output blocking capacitor?

...if not one on the input to next stage

Input dc base bias must be dc stiff, not affected by dc changes.

Set the ratio  $R_2/(R_1+R_2)$  to give 1.6v.

$R_{IN}C$  must pass relevant frequencies:

$\beta \times R_E$  is big, so  $Z_{in} \sim R_1 || R_2$

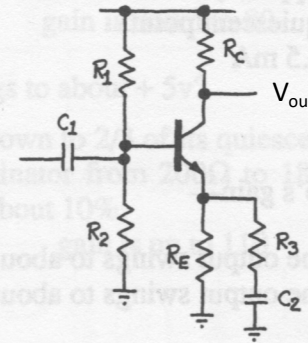


Figure X5.1: Skeleton Circuit

### Setting DC conditions

1. Choose  $R_C$  to center  $V_{out}$ , given  $I_{C(\text{quiescent})}$
2. Choose  $R_E$  to put  $V_E$  somewhere around 1 volt, for temperature stability
3. Let  $R_{Th}$  for the bias divider be about 1/10 ( $R_{in}$  transistor, which is  $\beta \cdot R_E$ ). As for the follower recently designed, the AC path to ground is to be ignored: the path through  $R_3$  is closed to DC, so invisible to the bias divider.
4. Choose  $R_1, R_2$  to put  $V_{base}$  at  $(V_E + 0.6V)$ .  $R_{Th}$  is roughly  $R_1$ , since the divider is so far unbalanced.

### Determining AC performance: Gain (what happens to signal)

1. Choose  $R_3$  (if any) for gain at quiescent point
2. Choose  $C_2$  for  $f_{3dB}$ : the relevant "R" is  $R_3 + r_e$
3. Choose  $C_1$  as usual; relevant "R" is circuit's  $Z_{in}$ , as usual: the circuit's AC input impedance, as for the follower: we look through capacitor  $C_2$ , and see  $R_3$  as a path to ground.

In choosing  $C_1$  we need to be generous, since two high-pass filters are at work: those using  $C_1$  and  $C_2$ . So, if we made the mistake of putting the  $f_{3dB}$  for each filter precisely at our target  $f_{3dB}$  for the *circuit*, we would be disappointed: we would find the *circuit's* response down 6dB.

## Impedances of an amp (or any component)...how to measure?

Treat amp as a Thevenin black box: *i.e.* a  $V_{th}$  in series with  $R_{th}$ .

$R_{in}$ : looking “forward,” into the input terminal.

$R_{out}$ : looking “backward,” into output terminal from next stage.

Measure the open circuit  $V_o = V_{th}$ .

Add a variable  $R$  in series (a substitution box is most convenient)

Change  $R$  until  $V$  across it is  $= \frac{1}{2} V_{th}$ .

Then,  $R_{th} = R$ .

## DVM vs VOM, for this application

DVM...10 M $\Omega$  input impedance...a FET input stage

hi-Z input, followed by op amp for feedback stability *vs.*

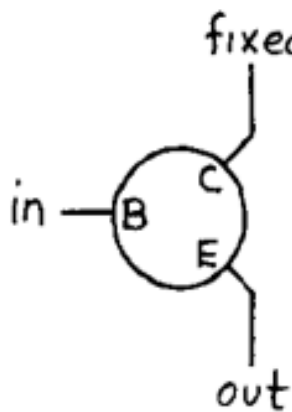
VOM...much lower input impedance, 20 k $\Omega$ /v...& variable at that!

Beware of body resistance,  $\sim 1\text{M}\Omega$ ,

*e.g.* don't short out a 10 M $\Omega$  instrument by your body fluids!

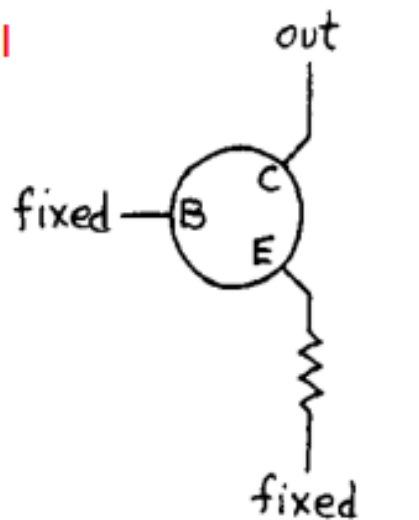
# Common transistor circuits...

recognized by where you take your output, where V fixed

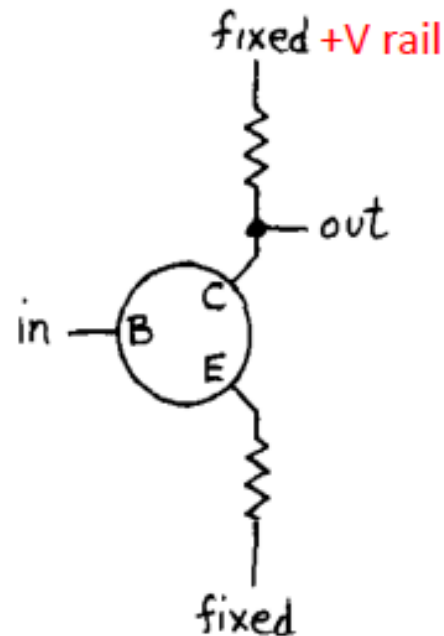


Emitter  
FOLLOWER

Current Amp

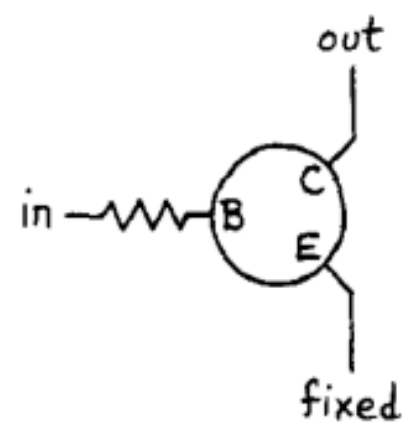


CURRENT SOURCE



Common Emitter  
AMPLIFIER

Voltage Amp



SWITCH