

READ p 90-93, 102, 115&6. Last week unfinished? Use make-up!
DO NOT DO: Lab 4-7,8; ONLY DO 5-2; optional 4-7.

Typical transistor: current gain " β " ~ 100 .

AC or DC

"**trans-(re)sistor**", an impedance matcher, look into each hole:

Look into input, want hi Z_{input} , easy to drive from previous.
x100 more than next stage.

gives 100x lower Z_{output} ideally: Z_{in} hi, Z_{out} low p96

Measuring Z: dial resistor box to reduce V by x2

Input voltage dynamic range:

set by 0.6v V_{BE} forward Si diode

Output voltage dynamic range (\equiv compliance):

p140

set by 2 voltage supply rails

X-ister switch: when "on", i_{CE} current saturated to get $V_{CE} \rightarrow 0$

Bias Rs set DC operating "sweet" spot, then optimize AC gain.

C_{in} & C_{out} block external offsets to preserve DC bias voltages

see Worked Exs. & assimilate pp 93

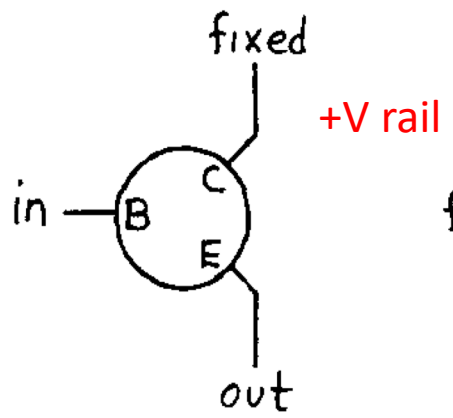
p90-3, 115-6

Next Monday's "must" reading:

Differential amps, FET's (field effect transistors): H&H 124-162

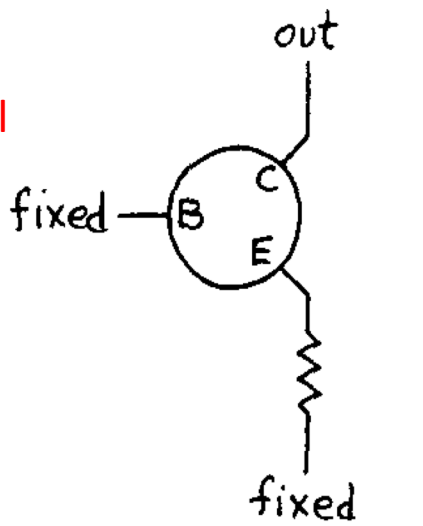
Your transistor circuits...

recognized by where you take your output, where V fixed

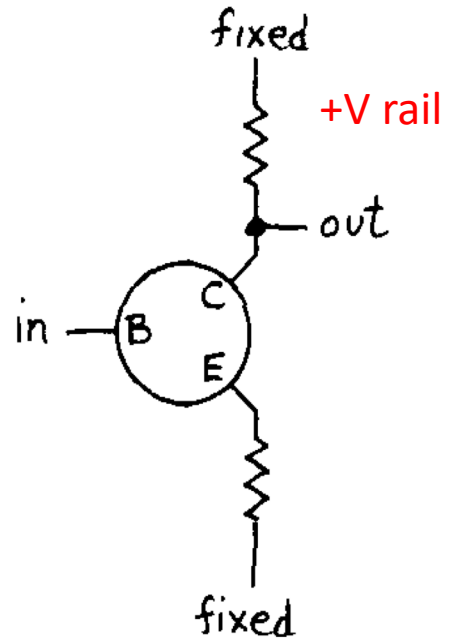


FOLLOWER
Emitter

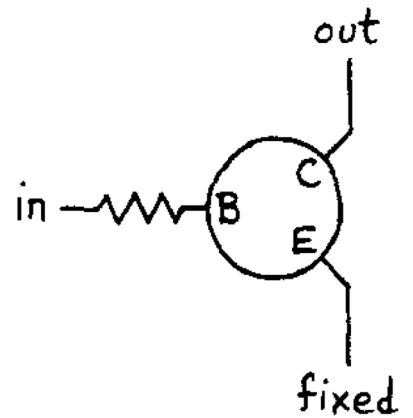
Impedance Matcher
Current Amp



CURRENT SOURCE



AMPLIFIER
Common Emitter
Voltage Amp



SWITCH

Steps in designing a transistor current amp \equiv impedance matcher

...the simplest is EMITTER FOLLOWER (non-inverting i amp):

Be sure to read p 90-93

(no hum)

5. Choose C_1
large enough
to put $f_{3dB} \approx 100\text{Hz}$
($R' = R_{Th}(\text{bias}) \parallel R_{in}(\text{base})$)

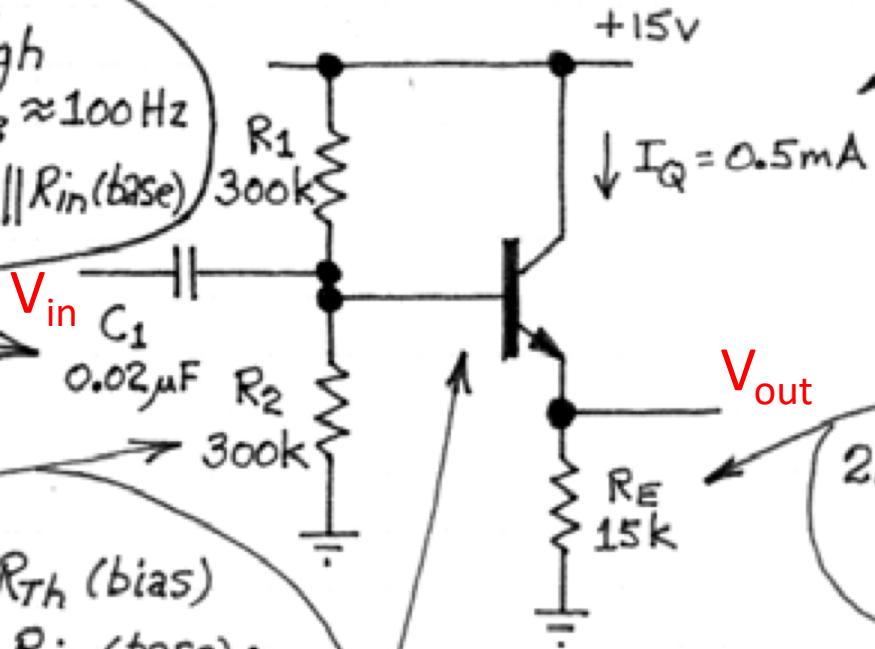
1. Choose I_Q

4. Let $R_{Th}(\text{bias})$
be $\ll R_{in}(\text{base})$;
 $R_{Th}(\text{base}) \approx \frac{1}{10} \beta \times 15\text{k}$
 ≈ 100

2. Choose R_E
to center V_E ,
given I_Q

3. Place V_B (quiescent)
around midpoint (7.5v),
roughly centering V_{out} (V_E).
This determines ratio $R_1:R_2$;
here $R_1 = R_2$

...but temp stability? touch it! linearity? low gain

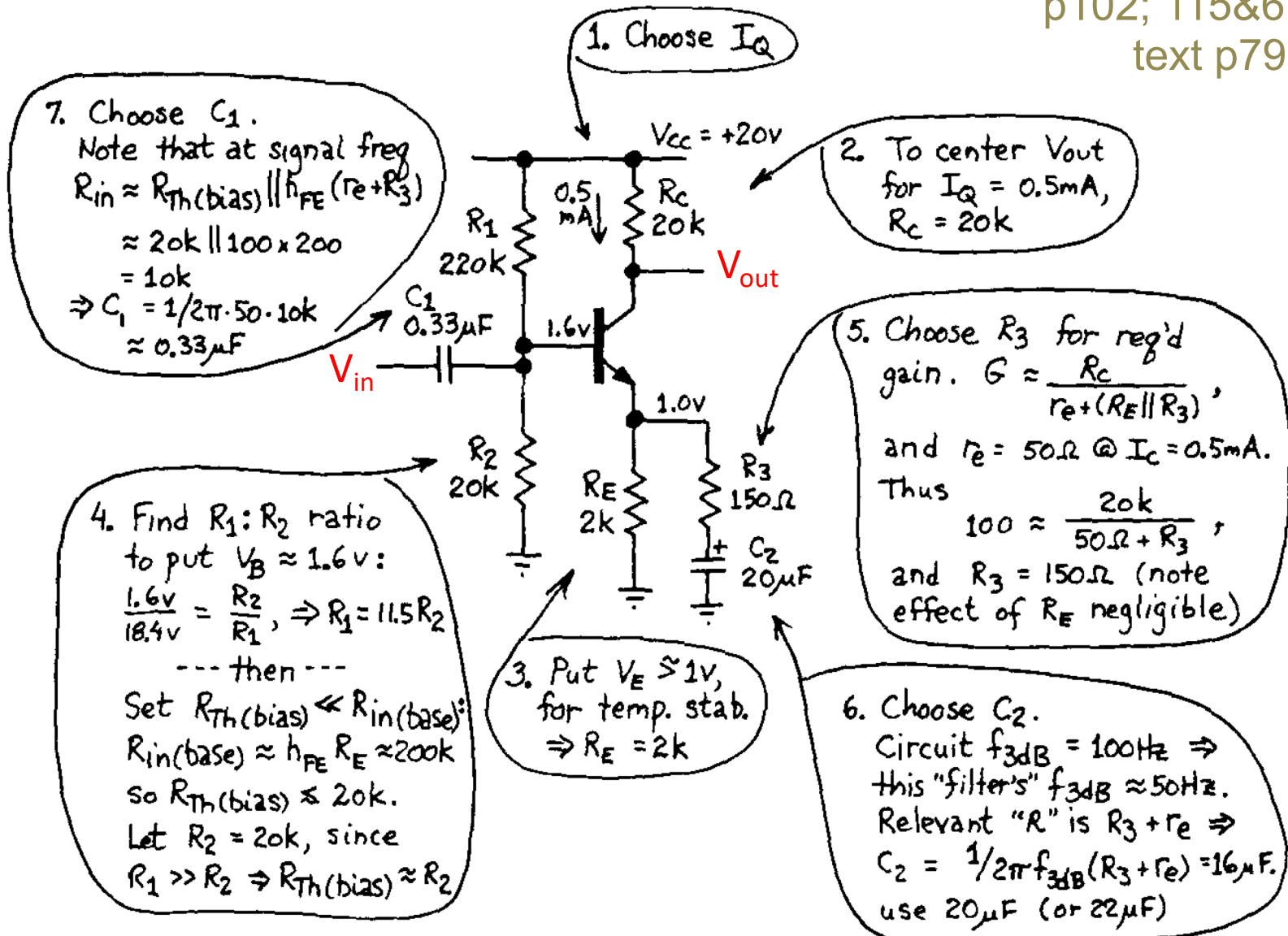


Design COMMON EMITTER amp: temp stability & hi AC gain, ~100:

DC Gain = $-R_C / R_E$, nice! Bypass R_E to get AC gain $> f_{3dB} \sim 100$ Hz (no hum).

Intrinsic, dynamic r_e , diode-like = $25\Omega / I_C(\text{mA})$. I_C quiescent = 0.5 mA

p102; 115&6
text p79



What to remember from Week 2?

Ratios: $\text{dB} = 10 \log_{10}(P_{\text{out}}/P_{\text{in}}) = 20 \log_{10}(V_{\text{out}}/V_{\text{in}})$...”2” since $P = V^2/R$
20 dB = x10 V ratio
6 dB = x 2 V ratio
3 dB = x0.707 V ratio = $(1/\sqrt{2}) = 1/2$ power point

Frequency domain (radians) $\omega_{3\text{dB}} = 2\pi f = 1/\tau$ p39
vs time domain (Hz) $f_{3\text{dB}} = \omega_{3\text{dB}}/2\pi$ p40

Filters
RC $\tau = RC$ time constant for $V_{\text{out}}/V_{\text{in}}$ to get to 0.63 of asymptote
 $\sim \text{k}\Omega \times \mu\text{fd} = \text{millisec (ms)} = \text{“audio” frequencies } 10\text{Hz}-20\text{k}$

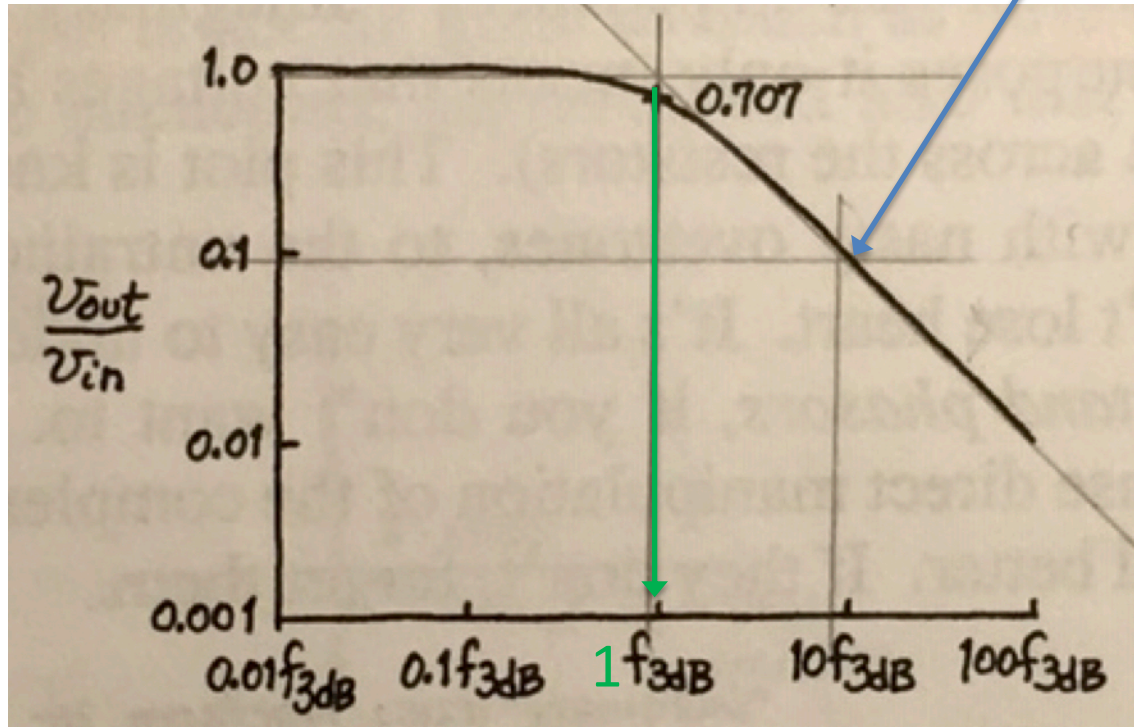
Rolloff response: 6dB/octave (20dB/decade) = x2 V drop per x2 freq, or 10×10
see Bode Plot

Hi (frequency) pass C = ac HF short, “bypasses” ac p41
Low f pass C = smoothing, “blocks” dc
3dB = down x2 in power (& 45° phase shift)

(Coils are a complement: Inductance $\tau = L/R$
C + L give resonance: Tank (resonant) circuit $\omega = 1/\sqrt{LC}$)

Bode frequency roll-off plot for a low-pass filter:
6 dB/octave = 20 dB/decade = -1 log-log slope
x2 for 2 x10 for 10 straight line

p41



RC filters – time domain vs frequency domain L/R ~same

3 dB ($0.707=1/\sqrt{2}$) inflection point for V_o/V_i
vs. 6 dB/octave (x2 for x2 in frequency) = 20 dB/decade rolloff in f
x2 for 2 x10 for 10

p39

Do not confuse these *frequency-domain* pictures with the earlier *RC* step-response picture, (which speaks in the *time-domain*).

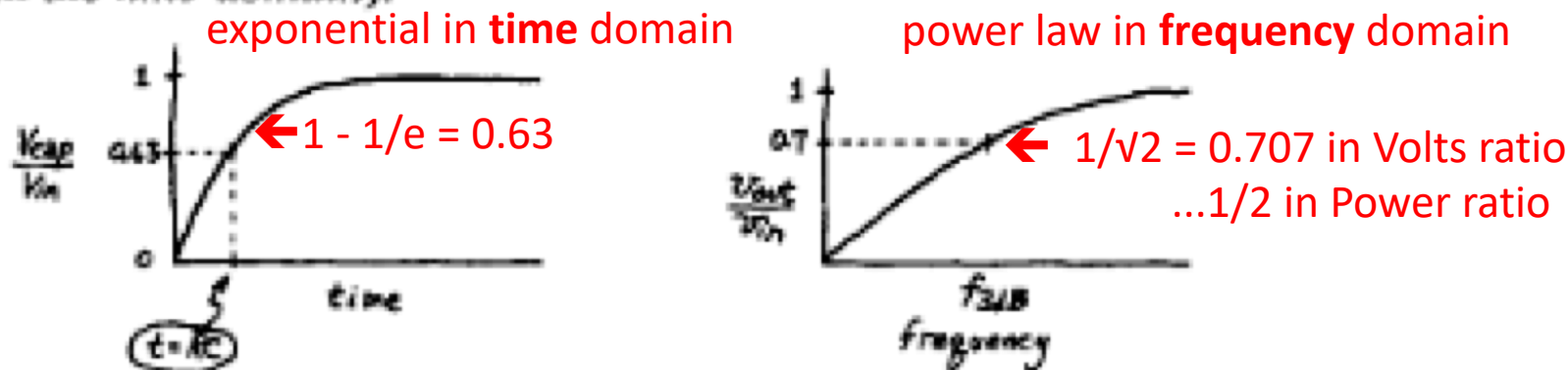


Figure N2.16: Deceptive similarity between shapes of time- and frequency- plots of RC circuits

Not only do the curves look vaguely similar. To make things worse, details here seem tailor-made to deceive you:

- ◆ *Step response*: in the *time RC* (time-constant), V_{cap} moves to about 0.6 of the applied step voltage (this is $1 - 1/e$).
- ◆ *Frequency domain*: at f_{3dB} , a frequency determined by RC , the filter's V_{out}/V_{in} is about 0.7 (this is $1/\sqrt{2}$)

Default scope etiquette...

ask for tutorial if at all in doubt

V_{in} to channel 1, zero at +2 vertical boxes

V_{out} to channel 2, zero at -2 vertical boxes

Causality \Rightarrow trigger on input

Horizontal trace starts at horizontal box 1

to see precursors

Choose time scale to display a couple of cycles

not too many, not too few

Trigger: normal, rising slope

~ never use “line” or “auto”

DC coupling...except to see DC offset

AC inserts a capacitor in the way

“Thou shall not touch trigger once its operational!!!”

“Only use ‘Auto’ in desperation to find the trace.”

Use a x10 probe if you need to minimize disturbance to circuit.

Compensate the probe adjusting its capacitance using a square wave;
it's Fourier transform has all frequencies.